



Real-time Computer Simulation of Three Dimensional Elastostatics using the Finite Point Method

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Need for the Present Work

- ❖ Real-time and realistic simulation of biological organs – for surgical simulators
- ❖ Use continuum mechanics based models for better realism
- ❖ Test the procedure on benchmark problems – beam, bar

Present Approach to Achieve the Speed Needed for Real-time Performance

- ✓ Use the simplified material behaviour – linear elastic
- ✓ Use Finite Point Method (FPM)
- ✓ Use a Graphics Processing Unit (GPU)

Governing Equations for Linear Elastostatics

$$(\lambda + \mu) \left\{ \frac{\partial^2 u_x}{\partial x^2} + \frac{\partial^2 u_y}{\partial x \partial y} + \frac{\partial^2 u_z}{\partial x \partial z} \right\} + \mu \left\{ \frac{\partial^2 u_x}{\partial x^2} + \frac{\partial^2 u_x}{\partial y^2} + \frac{\partial^2 u_x}{\partial z^2} \right\} = 0$$

$$(\lambda + \mu) \left\{ \frac{\partial^2 u_y}{\partial y^2} + \frac{\partial^2 u_x}{\partial x \partial y} + \frac{\partial^2 u_z}{\partial y \partial z} \right\} + \mu \left\{ \frac{\partial^2 u_y}{\partial x^2} + \frac{\partial^2 u_y}{\partial y^2} + \frac{\partial^2 u_y}{\partial z^2} \right\} = 0$$

$$(\lambda + \mu) \left\{ \frac{\partial^2 u_z}{\partial z^2} + \frac{\partial^2 u_x}{\partial x \partial z} + \frac{\partial^2 u_y}{\partial y \partial z} \right\} + \mu \left\{ \frac{\partial^2 u_z}{\partial x^2} + \frac{\partial^2 u_z}{\partial y^2} + \frac{\partial^2 u_z}{\partial z^2} \right\} = 0$$

$$\{\sigma\} = [D] \{\varepsilon\} \quad [D] = \begin{bmatrix} D_{11} & D_{12} & D_{12} & & & \\ D_{12} & D_{11} & D_{12} & & & \\ D_{12} & D_{12} & D_{11} & & & \\ & & & (D_{11} - D_{12})/2 & & \\ & & & & (D_{11} - D_{12})/2 & \\ & & & & & (D_{11} - D_{12})/2 \end{bmatrix}$$

$$\lambda = \frac{\nu E}{(1+\nu)(1-2\nu)} \quad \mu = \frac{E}{2(1+\nu)} \quad D_{11} = \frac{E(1-\nu)}{(1-2\nu)(1+\nu)} \quad D_{12} = \frac{E\nu}{(1-2\nu)(1+\nu)}$$

Finite Point Method (FPM)

(E. Onate, 2001, Computers and structures)

$$u(x) \cong \hat{u}(x) = \sum_{l=1}^m p_l(x) \alpha_l = \mathbf{p}(x)^T \boldsymbol{\alpha} \quad \text{-----(1)}$$

where $\boldsymbol{\alpha} = [\alpha_1, \alpha_2, \dots, \alpha_m]^T$

Function $u(x)$ can now be sampled at the n points belonging to Ω_i giving

$$\mathbf{u}^h = \begin{Bmatrix} u_1^h \\ u_2^h \\ \vdots \\ u_n^h \end{Bmatrix} \cong \begin{Bmatrix} \hat{u}_1 \\ \hat{u}_2 \\ \vdots \\ \hat{u}_n \end{Bmatrix} = \begin{Bmatrix} \mathbf{p}_1^T \\ \mathbf{p}_2^T \\ \vdots \\ \mathbf{p}_n^T \end{Bmatrix} \boldsymbol{\alpha} = \mathbf{C} \boldsymbol{\alpha} \quad \text{----(2)}$$

- In FPM, $n > m$ and hence approximation cannot fit nodal values.
- This problem can be overcome by determining the $u(x)$ values by minimizing the sum of the square distances of the error at each point weighted with a function $\varphi(x)$ as

$$J = \sum_{j=1}^n \varphi(x_j) (u_j^h - \hat{u}(x_j))^2 = \sum_{j=1}^n \varphi(x_j) (u_j^h - \mathbf{p}_j^T \boldsymbol{\alpha})^2 \quad \text{-----(3)}$$

with respect to the $\boldsymbol{\alpha}$ parameters. This approximation is termed weighted least square (WLS) interpolation.

Standard minimization of Eq (3) gives

$$\boldsymbol{\alpha} = \bar{\mathbf{C}}^{-1} \mathbf{u}^h, \quad \bar{\mathbf{C}}^{-1} = \mathbf{A}^{-1} \mathbf{B}, \quad \text{-----(4)}$$

$$\mathbf{A} = \sum_{j=1}^n \varphi(x_j) \mathbf{p}(x_j) \mathbf{p}^T(x_j), \quad \text{-----(5)}$$

$$\mathbf{B} = [\varphi(x_1) \mathbf{p}(x_1), \varphi(x_2) \mathbf{p}(x_2), \dots, \varphi(x_n) \mathbf{p}(x_n)]$$

Final approximation obtained by substituting α from Eq (4) into Eq (1):

$$\hat{u}(x) = \mathbf{p}^T \bar{\mathbf{C}}^{-1} \mathbf{u}^h = \mathbf{N}^T \mathbf{u}^h = \sum_{j=1}^n N_j^i u_j^h, \quad \text{-----}(6)$$

where the “shape functions” are

$$N_j^i(x) = \sum_{l=1}^m p_l(x) \bar{C}_{lj}^{-1} = \mathbf{p}^T(x) \bar{\mathbf{C}}^{-1}. \quad \text{-----}(7)$$

Discretization of governing equations

$$A(u_j) = 0 \quad \text{in } \Omega \quad \text{-----}(8)$$

with boundary conditions

$$u_j - \bar{u}_j = 0 \quad \text{on } \Gamma_u, \quad \text{-----}(9)$$

$$B(u_j) = 0 \quad \text{on } \Gamma_t. \quad \text{-----}(10)$$

Substituting Eq (6) in Eq (8), Eq (9) and Eq (10) and collocating the differential equation at each point in the analysis domain,

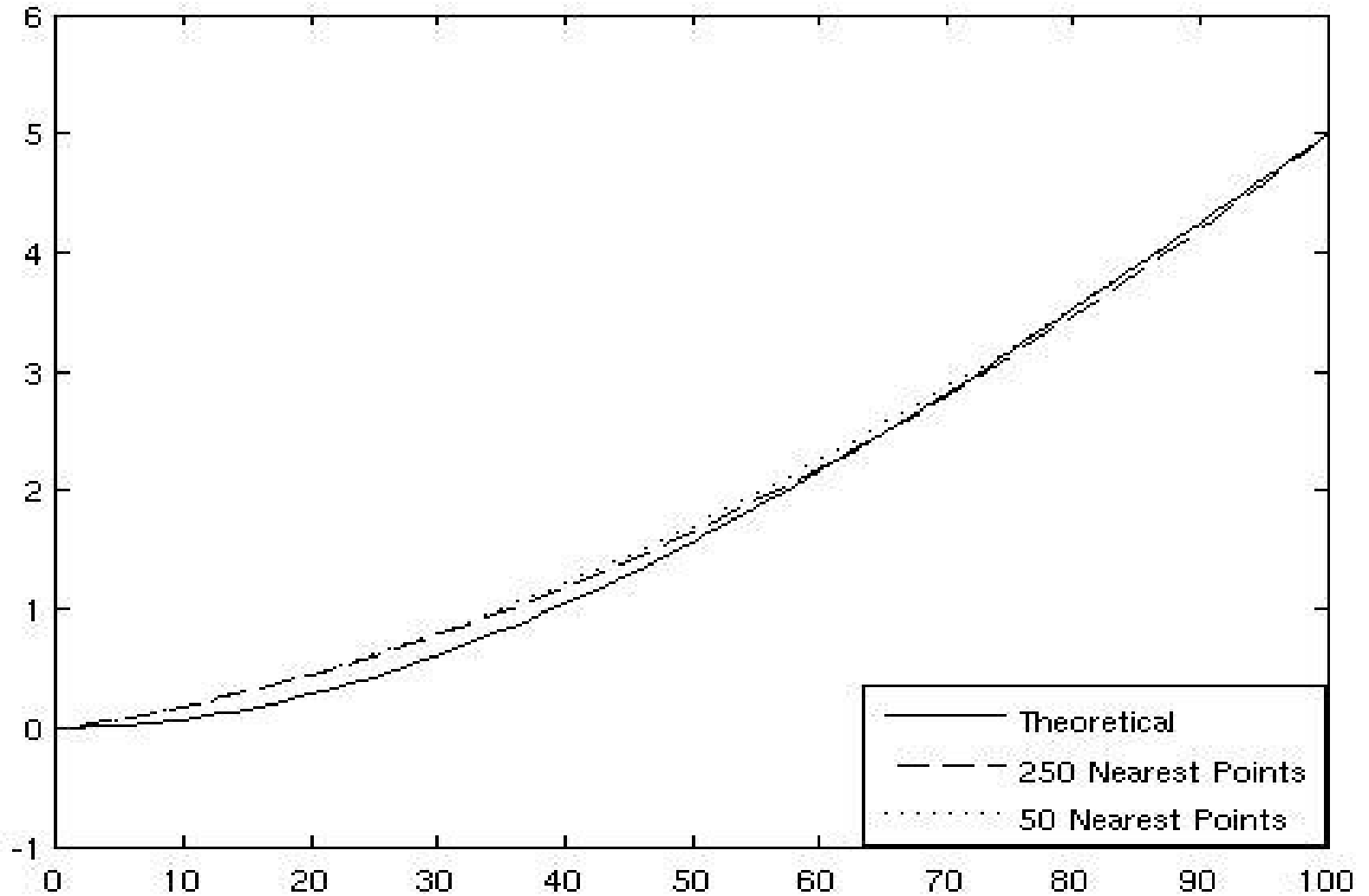
$$\begin{aligned} [A(\hat{u}_j)]_p &= 0 \quad p = 1, 2 \dots N_r, \\ \left[\hat{u}_j \right]_s - \bar{u}_j &= 0 \quad s = 1, 2 \dots N_u, \\ \left[B(\hat{u}_j) \right]_r &= 0 \quad r = 1, 2 \dots N_t. \end{aligned} \quad \text{-----(11)}$$

Sample Problem Description

A beam of length=99 mm and (4mmX4mm) cross section is discretized by uniformly spaced nodes located 1mm apart. Linear elastic material behaviour is assumed and strains and displacements are assumed small. $E=200000\text{N/mm}^2$, $\nu=0.33$

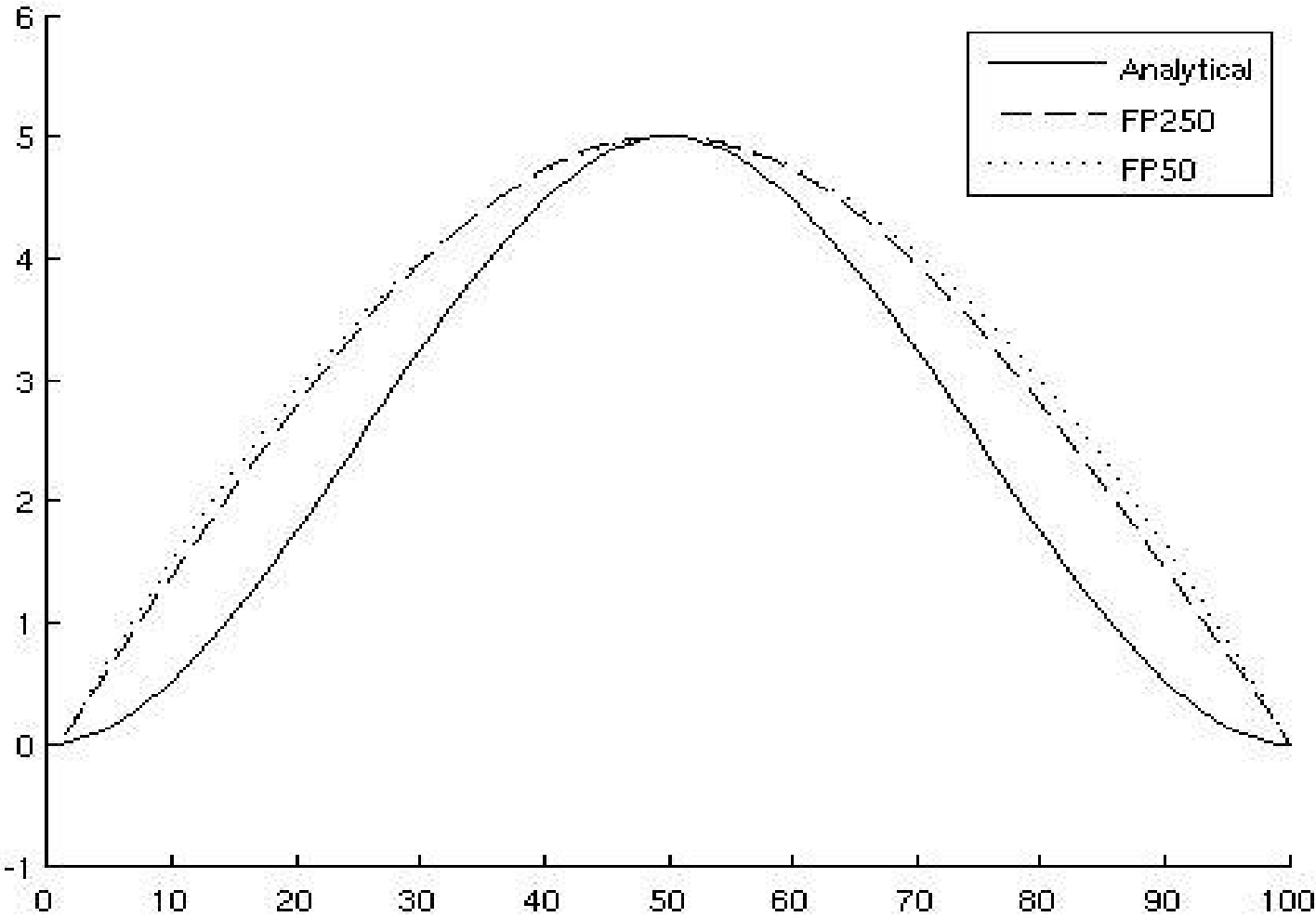
Results from FPM

Cantilever:

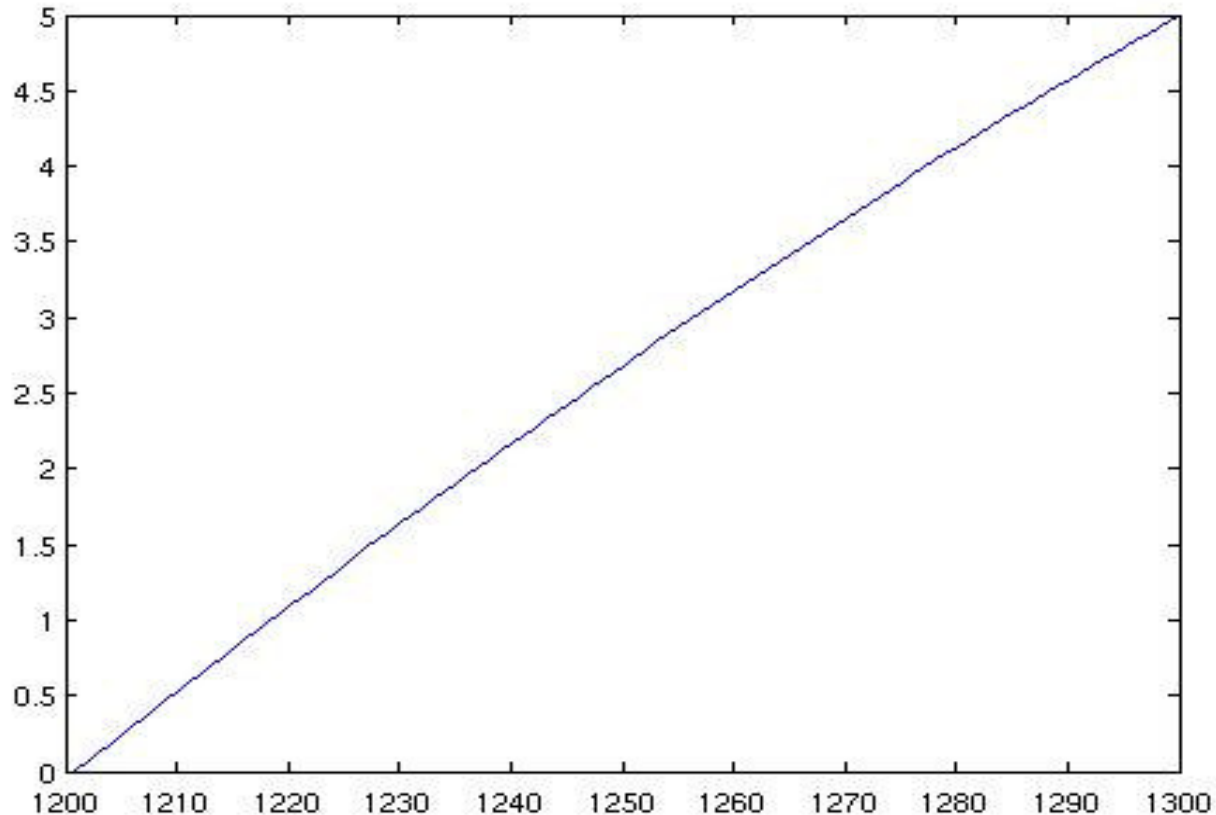


Theoretical formula: $y = (-1/6)(F/EI)(x^3 - 3l^2 x + 2l^3)$, x being measured from tip

Fixed at both ends:



Uniaxial tension:

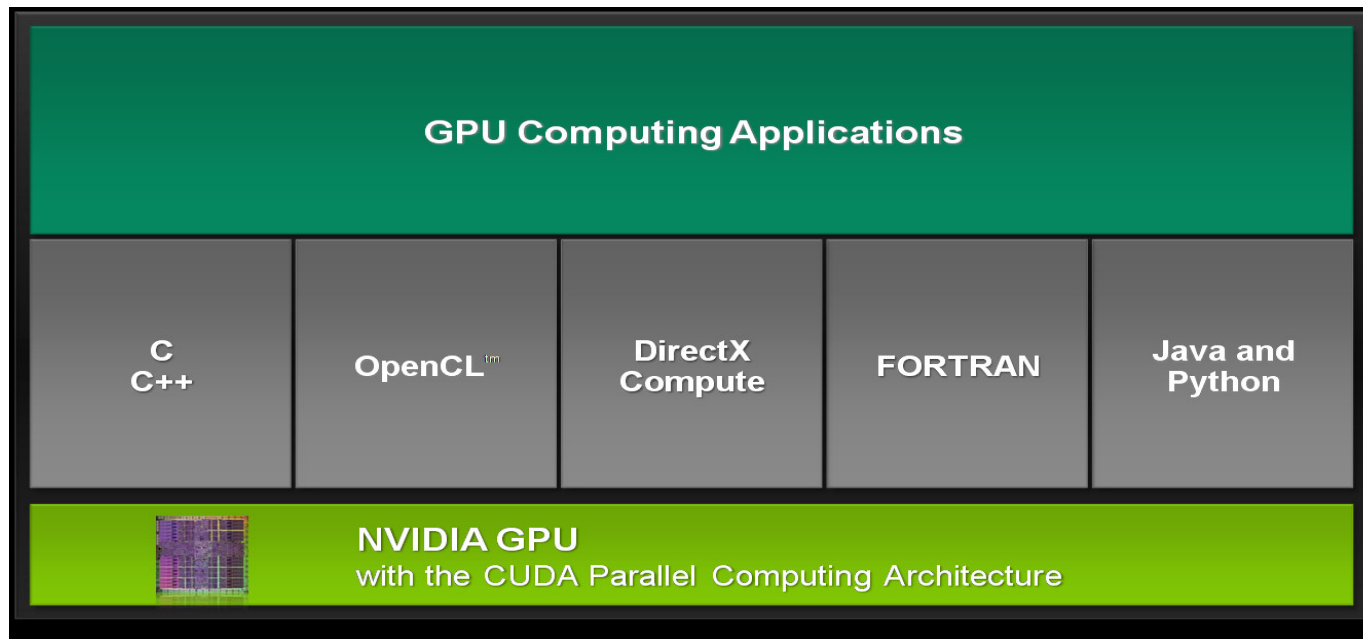
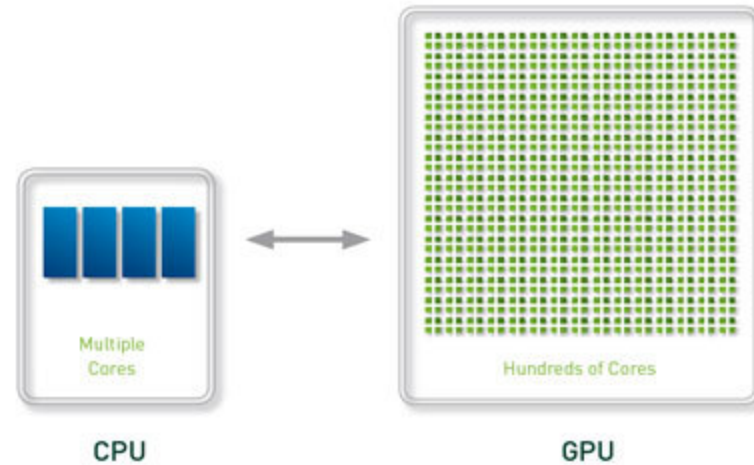


Truncated exponential weight function is used as the weight function:

$$w(r) = \frac{\exp(-r^2 / c^2) - \exp(-r_m^2 / c^2)}{1 - \exp(-r_m^2 / c^2)}$$

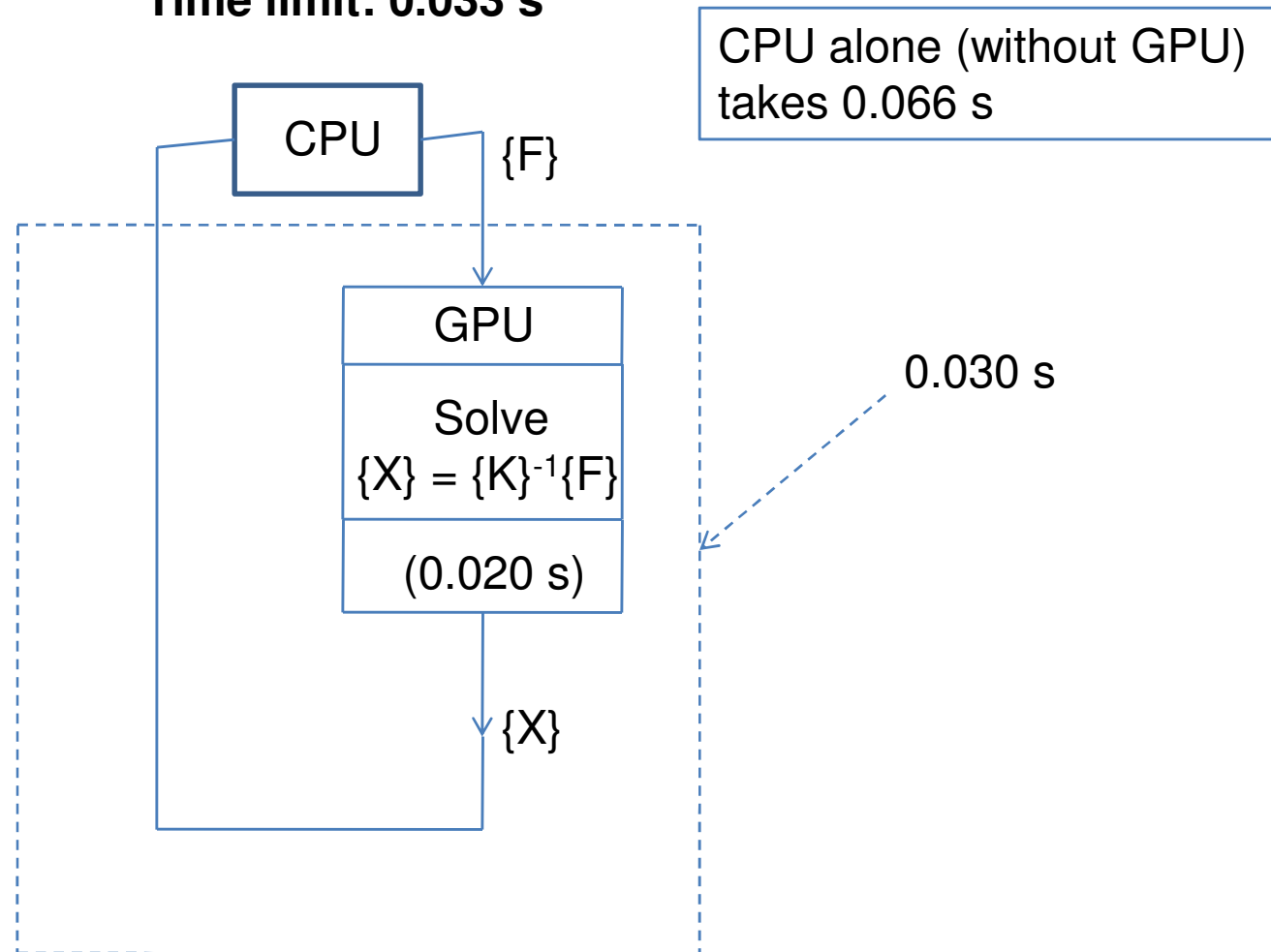
$$c = 0.25 r_{\max} \quad r_m = 2 r_{\max}$$

GPU (Images from www.nvidia.com)



Solution Strategy and Solution Times (GPU used: NVIDIA GeForce GTX 460)

Time limit: 0.033 s



(MATLAB and GPUmat are used for obtaining the results)

Conclusions

- CPU alone > Real-time not possible
- Real-time graphical simulation possible with GPU acceleration

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Thank You!